

The Open University of Sri Lanka

Faculty of Engineering Technology



Study Programme	: Bachelor of Technology (Engineering)
Name of the Examination	: Final Examination
Course Code and Title	: MEX 6278 / MEX 5230 – FLUID MECHANICS
Academic Year	: 2015/16
Date	: December 17, 2016
Time	: 9.30 hrs.-12.30 hrs.
Duration	: 3 hours

General Instructions

1. Read all instruction carefully before answering the questions.
2. This question paper consists of 8 questions. All questions carry equal marks.
3. Answer **any 5** questions only.

Q1.

- (a). By considering an infinitesimally small cubical fluid element, show that the general equation of continuity in three-dimensional space can be expressed as,

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{V}) = 0$$

where ,

$$\nabla = \frac{\partial}{\partial x} + \frac{\partial}{\partial y} + \frac{\partial}{\partial z} \quad \text{and} \quad \vec{V} = u\vec{i} + v\vec{j} + w\vec{k}$$

- (b). By using the above relationship, obtain the continuity equation for the following fluid flows.

- I. Steady flow
- II. Steady - Incompressible flow
- III. 2D - Compressible flow

- (c). The velocity components for X and Y directions of a steady incompressible flow are $u = x^2 + y^2 + z^2$ and $v = xy + yz + z$ respectively.

Find the velocity component (w) of the direction Z that requires to satisfy the continuity equation.

Q2.

- (a). Starting from Navier-Stokes equations, show that the velocity in steady laminar incompressible flow between two parallel plates, when upper plate moves at a velocity of U , in the direction of flow, is given by,

$$\frac{u}{U} = \frac{y}{a} - \frac{1}{2\mu} \frac{dp}{dx} (ay - y^2)$$

where,

a - distance between plates

μ - viscosity of the fluid

u - flow velocity at a height y from the bottom plate

- (b). Develop an expression for the total flow rate.

Q3.

- (a). Discuss the importance of the Reynolds number in relation to the behaviour of boundary layer.
- (b). Explain the significance of the boundary layer displacement thickness δ^* and the momentum thickness θ . Express δ^* and θ as integrals of the boundary layer velocity profiles on a smooth flat plate.
- (c). Calculate the ratio (δ^*/δ) for a laminar boundary layer with a velocity profile given by,

$$\frac{u}{U_\infty} = 2 \frac{y}{\delta} - \frac{y^2}{\delta^2}$$

- (d). Show that the frictional drag force per unit width (F_d) due to the boundary layer is given by,

$$F_d = \frac{2\delta}{15} \rho U_\infty^2$$

Q4.

- (a). By considering the velocity variation that causes rotation and angular deformation in two dimensional differential fluid element given in **Figure Q4**, show that the angular velocity of the fluid flow is given by,

$$\bar{\omega} = \frac{1}{2} \nabla \times \bar{V}$$

where, $\bar{\omega} = \omega_x \hat{i} + \omega_y \hat{j} + \omega_z \hat{k}$ and $\bar{V} = v_x \hat{i} + v_y \hat{j} + v_z \hat{k}$

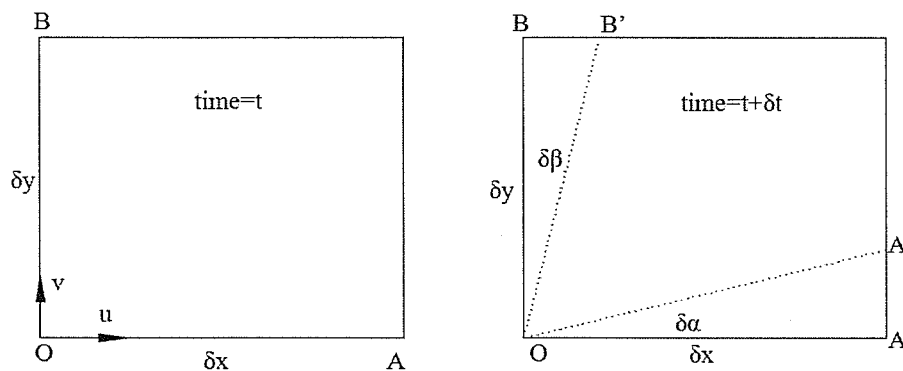


Figure Q4

- (b). A velocity field in a plane-flow is given by $V = 2yt \hat{i} + x \hat{j} \text{ ms}^{-1}$. Find the acceleration, angular velocity, and the vorticity vector at the point $(4\text{m}, 2\text{m})$ at $t = 3 \text{ sec}$.

Q5.

- (a). What do you understand by potential flow? Briefly explain some applications of potential flow theory.
- (b). State the properties of a fluid flow that are required to exist a stream function.
- (c). In a two-dimensional incompressible flow, the fluid velocity components are given by: $\mathbf{u} = x - 4y$ and $\mathbf{v} = -y - 4x$. Show that the flow satisfies the continuity equation. Obtain the expression for the stream function. If the flow is potential, obtain the expression for the velocity potential.

Q6.

- (a). What do you understand by complex potential and complex velocity?
- (b). What is a stagnation point?
- (c). Show that the equation of the streamlines due to uniform line sources of strength Q through the points $A(-a,0)$, $B(a,0)$ and a uniform line sink of strength $2Q$ through the origin as depicted in **Figure Q6** is given by,

$$(x^2 - y^2)^2 = 2kxya^2$$

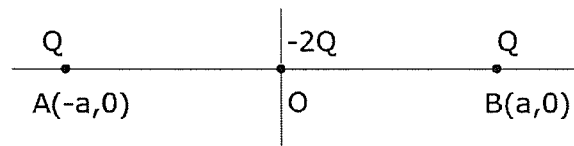


Figure Q6

Q7.

- (a). State the assumptions that is required to derive the Reynolds equation.
- (b). **Figure Q7** describes the geometry of a step bearing. Simplify the Reynolds equation for this application and show that the pressure variation on *section -1* and *section -2* can be expressed as,

$$P_1(x) = 2P_{\max} \frac{x}{L}$$

$$P_2(x) = 2P_{\max} \left(1 - \frac{x}{L}\right)$$

where, P_{\max} is the pressure at $x=L/2$

- (c). By applying continuity equation, show that,

$$P_{\max} = \frac{3u\eta L(h_1 - h_2)}{(h_1^3 + h_2^3)}$$

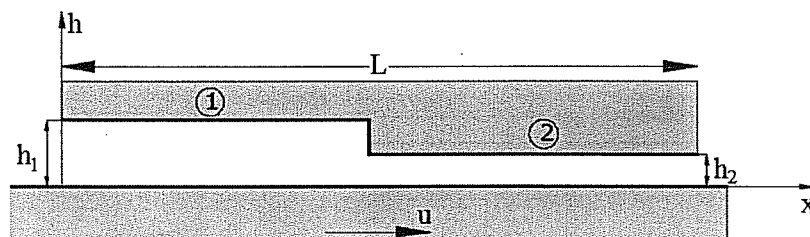


Figure Q7

Q8.

(a). By using suitable examples, explain dimensional homogeneity, geometric similarity, kinematic similarity and dynamic similarity.

(b). State Buckingham π theorem.

(c). By using Buckingham π theorem, show that the frictional torque T of a disc of diameter D rotating at a speed N in a fluid of viscosity μ and density ρ in a turbulent flow is given by,

$$T = D^5 N^2 \rho \phi \left(\frac{\mu}{D^2 N \rho} \right)$$

(d). A disk of **90mm** in diameter rotates in water having $\rho=1000\text{kg/m}^3$ and $\mu=10^{-3}\text{Ns/m}^2$ requires a torque of **0.77 J**. Find the torque required for a similar disc of **240mm** diameter rotating at **3000 rev/min** in air having $\rho=1.2\text{kg/m}^3$ and $\mu=1.8 \times 10^{-5}\text{Ns/m}^2$.

Navier-Stokes equations for incompressible flow:-

$$\rho \left(\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} \right) = \rho g_x - \frac{\partial p}{\partial x} + \mu \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right)$$

$$\rho \left(\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} \right) = \rho g_y - \frac{\partial p}{\partial y} + \mu \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} + \frac{\partial^2 v}{\partial z^2} \right)$$

$$\rho \left(\frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} \right) = \rho g_z - \frac{\partial p}{\partial z} + \mu \left(\frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial y^2} + \frac{\partial^2 w}{\partial z^2} \right)$$

Frictional drag force per unit width due to laminar boundary layer:- $F_d = \rho \int_0^{\delta} u(U_{\infty} - u) dy$

Reynolds equation:-

$$\frac{\partial}{\partial x} \left(\frac{h^3}{12\eta} \frac{\partial p}{\partial x} \right) + \frac{\partial}{\partial y} \left(\frac{h^3}{12\eta} \frac{\partial p}{\partial y} \right) = \frac{(u_h + u_0)}{2} \frac{\partial(\rho h)}{\partial x} + \frac{(v_h + v_0)}{2} \frac{\partial(\rho h)}{\partial y} + \frac{\partial(\rho h)}{\partial t}$$

Acceleration vector:- $\vec{a} = \frac{d\vec{V}}{dt} = \frac{\partial \vec{V}}{\partial t} + u \frac{\partial \vec{V}}{\partial x} + v \frac{\partial \vec{V}}{\partial y} + w \frac{\partial \vec{V}}{\partial z}$

- End -