00160

THE OPEN UNIVERSITY OF SRI LANKA

BACHELOR OF TECHNOLOGY – LEVEL 05

FINAL EXAMINATION – 2011/2012

MPZ 5230 – ENGINEERING MATHEMATICS III

DURATION: THREE (03) HOURS

Date: 28th February 2012 **Time: 0930hrs – 1230hrs**

Instructions:

- Answer only six (06) questions.
- No of pages in the paper – 04.
- State any assumptions you required.
- Do not spend more than 30 minutes for any problem.
- Show all your workings.
- All symbols are in standard notation.

01. a) Evaluate the following integral by changing to polar co-ordinates.

$$\int_0^a \int_0^{\sqrt{a^2-y^2}} (x^2 + y^2)\, dx\, dy$$

b) Write down the spherical polar co-ordinates of the point $P = (x, y, z)$

Find the flux of $\underline{F} = xz^2\, \underline{i} + (x^2y - z^3)\, \underline{j} + (2xy + y^2 z)\, \underline{k}$ outwards across the entire surfacce of the hemispherical region bounded by $z = (a^2 - x^2 - y^2)^{1/2}$ and $z = 0$. (Hint: use spherical polar co-ordinates)

02. a) State Gauss Divergence theorem.

b) Verify the Divergence theorem for $\underline{A} = 2y^2\, \underline{i} - z^2\, \underline{j} + x\, \underline{k}$ taken over the region in the first octant bounded by $y^2 + z^2 = 9, x = 0$ *and* $x = 2$.

03. a) State the Stoke's theorem.

b) Verify Stoke's theorem for $\underline{F} = xz\, \underline{i} - y\, \underline{j} + x^2 y\, \underline{k}$, where s is the surface of the region bounded by $x = 0, y = 0, z = 0$ *and* $2x + y + 2z = 8$, which is not included in the *xz* plane.

04. a) Find the image of the rectangular region in z plane bounded by straight lines $x = 1, x = 2, y = 1, y = 2$ under the mapping $w = {}^{1}/_{z}$.

b) Plot the image of the region, $1 < x < 2$, under the mapping $w = z^2$.

c) Expand the following function in Laurent's series $\frac{1}{z(z+2)^3}$ *about* $z = -2$.

05. a) i) Find the region of convergence of the following series.

$$\sum_{n=1}^{\infty} \frac{(z+2)^{n-1}}{(n+1)^3 \cdot 4^n}$$

ii) Find the Taylor series of the given function with given point as centre and determine the radius of convergence $\frac{1}{(1-z)}$, i

b) i) Consider the function $f(z) = \frac{e^z}{(z-1)(z+3)^2}$ and identify the singularities of $f(z)$.

ii) Find all the residues of the function $f(z)$.

iii) Evaluate the integral $\int_c f(z)\,dz$, where c is the contour $|z| = {}^{3}/_{2}$.

06 a) Define the transformation law for vectors.

Let a transformation from a co-ordinate system x_i to a co-ordinate system x_i' be defind by the transformation law, where the direction cosines are in the matrix form;

$$\alpha_{ij} = \begin{bmatrix} {}^{\sqrt{5}}/_{3} & {}^{\sqrt{5}}/_{3} & -{}^{\sqrt{5}}/_{3} \\ {}^{\sqrt{3}}/_{2} & -{}^{\sqrt{3}}/_{2} & 0 \\ {}^{\sqrt{7}}/_{6} & {}^{\sqrt{7}}/_{6} & 2{}^{\sqrt{7}}/_{6} \end{bmatrix}$$

b) Find the components of the vector $\underline{A} = 3\,\underline{i}_1 + 6\,\underline{i}_2 + 3\,\underline{i}_3$ in the x_i' co-ordinate system.

c) Find the components of the vector $\underline{B'} = \sqrt{5}\underline{i}_1' + \sqrt{3}\underline{i}_2' + \sqrt{7}\underline{i}_3'$ in the x_i co-ordinate system.

d) Determine the components of the vector product of $\underline{A}$ and $\underline{B}$ in the x_i' co-ordinate system.

07. Consider the second order symmetric tensor whose components are given by;

$$T_{ij} = \begin{bmatrix} 1 & 1 & 3 \\ 1 & 1 & -3 \\ 3 & -3 & -3 \end{bmatrix}$$

a) Find the eigen values and the principal axes of the tensor.

b) Express the tensor with respect to its principal axes.

c) Write the equation of the transformation relating to the co-ordinates x_i with that determined by the principal axes.

d) Verify the results in (b) by using the transformation law for second order tensor.

08. Using the variable seperable method, find the solution of the heat equation

$u_t = k\, u_{xx}$ for $0 < x < L$, subject to boundary conditions.

$u(0,t) = 0$ and $u(L,t) = 0$ for $t > 0$ and an initial condition.

$$u(x,0) = \begin{cases} T_0 & 0 \le x \le L/2 \\ 0 & L/2 \le x \le L \end{cases}$$

Explain briefly the physical situation represented by the equation above.

09. a) Define Fourier transformation and inverse Fourier transformation.

b) Find the Fourier transform of $f(x)$ if

$$f(x) = \begin{cases} 1 - x^2 ; & |x| \le 1 \\ 0 ; & |x| > 1 \end{cases}$$

c) i) Write the Fourier sine transform and Fourier cosine transform of a function.

ii) Find the Fourier cosine transforms of e^{-mx}, $m > 0$. Hence show that

$$\int_0^\infty \frac{\cos pv}{v^2 + \beta^2}\, dv = \frac{\pi}{2\beta}\, e^{-p\beta} \quad (p > 0, \beta > 0)$$

10. The following data represents the price of certain commodity was obtained in each of the four towns A, B, C and D in four quarters of the year. The prices are given below.

Quarter	Towns			
	A	B	C	D
1	60	50	60	50
2	50	40	65	50
3	45	35	45	50
4	65	45	60	70

a) Explain briefly the technique of analysis of variance of data with one way classification.

b) Test whether the means of the prices between different towns, significantly different among themselves.

11. A company manufactures two products A and B. These products are processed in the same machine. It takes 10 minutes to process one unit of product A and 2 minutes for each unit of product B and the machine operates for a maximum of 35 hrs in a week. Product A requires 1kg and B 0.5 kg of raw material per unit the supply of which is 600 kg per week. Market constarint on product B is known to be 800 unit every week. Product A costs Rs.5 per unit and sold at Rs.10. Product B costs Rs.6 per unit and can be sold in the market at a unit price of Rs.8.

a) Formulate as Linear Programming Problem (L.P.P).

b) Find maximum profit by using graphical method.

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ν_2 \ ν_1	1	2	3	4	5	6	7	8	9	10	12	15	20	24	30	40	60	120	∞
1	161.4	199.5	215.7	224.6	230.2	234.0	236.8	238.9	240.5	241.9	243.9	245.9	248.0	249.1	250.1	251.1	252.2	253.3	254.3
2	18.51	19.00	19.16	19.25	19.30	19.33	19.35	19.37	19.38	19.40	19.41	19.43	19.45	19.45	19.46	19.47	19.48	19.49	19.50
3	10.13	9.55	9.28	9.12	9.01	8.94	8.89	8.85	8.81	8.79	8.74	8.70	8.66	8.64	8.62	8.59	8.57	8.55	8.53
4	7.71	6.94	6.59	6.39	6.26	6.16	6.09	6.04	6.00	5.96	5.91	5.86	5.80	5.77	5.75	5.72	5.69	5.66	5.63
5	6.61	5.79	5.41	5.19	5.05	4.95	4.88	4.82	4.77	4.74	4.68	4.62	4.56	4.53	4.50	4.46	4.43	4.40	4.36
6	5.99	5.14	4.76	4.53	4.39	4.28	4.21	4.15	4.10	4.06	4.00	3.94	3.87	3.84	3.81	3.77	3.74	3.70	3.67
7	5.59	4.74	4.35	4.12	3.97	3.87	3.79	3.73	3.68	3.64	3.57	3.51	3.44	3.41	3.38	3.34	3.30	3.27	3.23
8	5.32	4.46	4.07	3.84	3.69	3.58	3.50	3.44	3.39	3.35	3.28	3.22	3.15	3.12	3.08	3.04	3.01	2.97	2.93
9	5.12	4.26	3.86	3.63	3.48	3.37	3.29	3.23	3.18	3.14	3.07	3.01	2.94	2.90	2.86	2.83	2.79	2.75	2.71
10	4.96	4.10	3.71	3.48	3.33	3.22	3.14	3.07	3.02	2.98	2.91	2.85	2.77	2.74	2.70	2.66	2.62	2.58	2.54
11	4.84	3.98	3.59	3.36	3.20	3.09	3.01	2.95	2.90	2.85	2.79	2.72	2.65	2.61	2.57	2.53	2.49	2.45	2.40
12	4.75	3.89	3.49	3.26	3.11	3.00	2.91	2.85	2.80	2.75	2.69	2.62	2.54	2.51	2.47	2.43	2.38	2.34	2.30
13	4.67	3.81	3.41	3.18	3.03	2.92	2.83	2.77	2.71	2.67	2.60	2.53	2.46	2.42	2.38	2.34	2.30	2.25	2.21
14	4.60	3.74	3.34	3.11	2.96	2.85	2.76	2.70	2.65	2.60	2.53	2.46	2.39	2.35	2.31	2.27	2.22	2.18	2.13
15	4.54	3.68	3.29	3.06	2.90	2.79	2.71	2.64	2.59	2.54	2.48	2.40	2.33	2.29	2.25	2.20	2.16	2.11	2.07
16	4.49	3.63	3.24	3.01	2.85	2.74	2.66	2.59	2.54	2.49	2.42	2.35	2.28	2.24	2.19	2.15	2.11	2.06	2.01
17	4.45	3.59	3.20	2.96	2.81	2.70	2.61	2.55	2.49	2.45	2.38	2.31	2.23	2.19	2.15	2.10	2.06	2 01	1.96
18	4.41	3.55	3.16	2.93	2.77	2.66	2.58	2.51	2.46	2.41	2.34	2.27	2.19	2.15	2.11	2.06	2.02	1.97	1.92
19	4.38	3.52	3.13	2.90	2.74	2.63	2.54	2.48	2.42	2.38	2.31	2.23	2.16	2.11	2.07	2.03	1.98	1.93	1.88
20	4.35	3.49	3.10	2.87	2.71	2.60	2.51	2.45	2.39	2.35	2.28	2.20	2.12	2.08	2.04	1.99	1.95	1.90	1.84
21	4.32	3.47	3.07	2.84	2.68	2.57	2.49	2.42	2.37	2.32	2.25	2.18	2.10	2 05	2.01	1.96	1.92	1.87	1.81
22	4.30	3.44	3.05	2.82	2.66	2.55	2.46	2.40	2.34	2.30	2.23	2.15	2.07	2.03	1.98	1.94	1.89	1.84	1.78
23	4.28	3.42	3.03	2.80	2.64	2.53	2.44	2 37	2.32	2.27	2.20	2.13	2.05	2.01	1.96	1.91	1.86	1.81	1.76
24	4.26	3.40	3.01	2.78	2.62	2.51	2.42	2.36	2.30	2.25	2.18	2.11	2.03	1.98	1.94	1.89	1.84	1.79	1.73
25	4.24	3.39	2.99	2.76	2.60	2.49	2.40	2.34	2.28	2.24	2.16	2.09	2.01	1.96	1.92	1 87	1.82	1.77	1.71
26	4.23	3.37	2.98	2.74	2.59	2.47	2.39	2.32	2.27	2.22	2.15	2.07	1.99	1.95	1.90	1.85	1.80	1.75	1.69
27	4.21	3.35	2.96	2.73	2.57	2.46	2.37	2.31	2.25	2.20	2.13	2.06	1 97	1.93	1.88	1 84	1.79	1.73	1.67
28	4.20	3.34	2.95	2.71	2.56	2.45	2.36	2.29	2.24	2.19	2.12	2.04	1.96	1.91	1.87	1.82	1.77	1.71	1.65
29	4.18	3.33	2.93	2.70	2.55	2.43	2.35	2.28	2.22	2.18	2.10	2.03	1.94	1.90	1.85	1.81	1.75	1.70	1.64
30	4.17	3.32	2.92	2.69	2.53	2.42	2.33	2.27	2.21	2.16	2.09	2.01	1.93	1.89	1.84	1.79	1.74	1.68	1.62
40	4.08	3.23	2.84	2.61	2.45	2.34	2.25	2.18	2.12	2.08	2.00	1.92	1.84	1.79	1.74	1.69	1.64	1.58	1 51
60	4.00	3.15	2.76	2.53	2.37	2.25	2.17	2.10	2.04	1.99	1.92	1.84	1.75	1.70	1.65	1 59	1.53	1.47	1.39
120	3.92	3.07	2.68	2.45	2.29	2.17	2.09	2.02	1.96	1.91	1.83	1.75	1.66	1.61	1.55	1.50	1.43	1.35	1 25
∞	3.84	3.00	2.60	2.37	2.21	2.10	2.01	1.94	1.88	1.83	1.75	1.67	1.57	1.52	1.46	1.39	1.32	1.22	1.00

ν_1 and ν_2 are the number of degrees of freedom in the numerator and denominator respectively.

The probability of F exceeding the entry value is in all cases 5%.

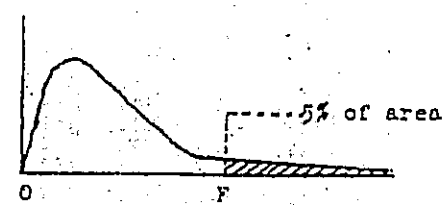


TABLE 01.4(A) : PERCENTAGE POINTS OF THE F DISTRIBUTION (UPPER 5% TAIL)

00160

00160

v_2 \ v_1	1	2	3	4	5	6	7	8	9	10	12	15	20	24	30	40	60	120	∞
1	405300	500000	540400	562500	576400	585900	592900	598100	602300	605600	610700	615800	620900	623500	626100	628700	631300	634000	636600
2	998.5	999.0	999.2	999.2	999.3	999.3	999.4	999.4	999.4	999.4	999.4	999.4	999.4	999.5	999.5	999.5	999.5	999.5	999.5
3	167.0	148.5	141.1	137.1	134.6	132.8	131.6	130.6	129.9	129.2	128.3	127.4	126.4	125.9	125.4	125.0	124.5	124.0	123.5
4	74.14	61.25	56.18	53.44	51.71	50.53	49.66	49.00	48.47	48.05	47.41	46.76	46.10	45.77	45.43	45.09	44.75	44.40	44.05
5	47.18	37.12	33.20	31.09	29.75	28.84	28.16	27.64	27.24	26.92	26.42	25.91	25.39	25.14	24.87	24.60	24.33	24.06	23.79
6	35.51	27.00	23.70	21.92	20.81	20.03	19.46	19.03	18.69	18.41	17.99	17.56	17.12	16.89	16.67	16.44	16.21	15.99	15.75
7	29.25	21.69	18.77	17.19	16.21	15.52	15.02	14.63	14.33	14.08	13.71	13.32	12.93	12.73	12.53	12.33	12.12	11.91	11.70
8	25.42	18.49	15.83	14.39	13.49	12.86	12.40	12.04	11.77	11.54	11.19	10.84	10.48	10.30	10.11	9.92	9.73	9.53	9.33
9	22.86	16.39	13.90	12.56	11.71	11.13	10.70	10.37	10.11	9.89	9.57	9.24	8.90	8.72	8.55	8.37	8.19	8.00	7.81
10	21.04	14.91	12.55	11.28	10.48	9.92	9.52	9.20	8.96	8.75	8.45	8.13	7.80	7.64	7.47	7.30	7.12	6.94	6.76
11	19.69	13.81	11.56	10.35	9.58	9.05	8.66	8.35	8.12	7.92	7.63	7.32	7.01	6.85	6.68	6.52	6.35	6.17	6.00
12	18.64	12.97	10.80	9.63	8.89	8.38	8.00	7.71	7.48	7.29	7.00	6.71	6.40	6.25	6.09	5.93	5.76	5.59	5.42
13	17.81	12.31	10.21	9.07	8.35	7.86	7.49	7.21	6.98	6.80	6.52	6.23	5.93	5.78	5.63	5.47	5.30	5.13	4.97
14	17.14	11.78	9.73	8.62	7.92	7.43	7.08	6.80	6.58	6.40	6.13	5.85	5.56	5.41	5.25	5.10	4.94	4.77	4.60
15	16.59	11.34	9.34	8.25	7.57	7.09	6.74	6.47	6.26	6.08	5.81	5.54	5.25	5.10	4.95	4.80	4.64	4.47	4.31
16	16.12	10.97	9.00	7.94	7.27	6.81	6.46	6.19	5.98	5.81	5.55	5.27	4.99	4.85	4.70	4.54	4.39	4.23	4.06
17	15.72	10.66	8.73	7.68	7.02	6.56	6.22	5.96	5.75	5.58	5.32	5.05	4.78	4.63	4.48	4.33	4.18	4.02	3.85
18	15.38	10.39	8.49	7.46	6.81	6.35	6.02	5.76	5.56	5.39	5.13	4.87	4.59	4.45	4.30	4.15	4.00	3.84	3.67
19	15.08	10.16	8.28	7.26	6.62	6.18	5.85	5.59	5.39	5.22	4.97	4.70	4.43	4.29	4.14	3.99	3.84	3.68	3.51
20	14.82	9.95	8.10	7.10	6.46	6.02	5.69	5.44	5.24	5.08	4.82	4.56	4.29	4.15	4.00	3.86	3.70	3.54	3.38
21	14.59	9.77	7.94	6.95	6.32	5.88	5.56	5.31	5.11	4.95	4.70	4.44	4.17	4.03	3.88	3.74	3.58	3.42	3.26
22	14.38	9.61	7.80	6.81	6.19	5.76	5.44	5.19	4.99	4.83	4.58	4.33	4.06	3.92	3.78	3.63	3.48	3.32	3.15
23	14.19	9.47	7.67	6.69	6.08	5.65	5.33	5.09	4.89	4.73	4.48	4.23	3.96	3.82	3.68	3.53	3.38	3.23	3.05
24	14.03	9.34	7.55	6.59	5.98	5.55	5.23	4.99	4.80	4.64	4.39	4.14	3.87	3.74	3.59	3.45	3.29	3.14	2.97
25	13.88	9.22	7.45	6.49	5.88	5.46	5.15	4.91	4.71	4.56	4.31	4.06	3.79	3.66	3.52	3.37	3.22	3.06	2.89
26	13.74	9.12	7.36	6.41	5.80	5.38	5.07	4.83	4.64	4.48	4.24	3.99	3.72	3.59	3.44	3.30	3.15	2.99	2.82
27	13.61	9.02	7.27	6.33	5.73	5.31	5.00	4.76	4.57	4.41	4.17	3.92	3.66	3.52	3.38	3.23	3.08	2.92	2.75
28	13.50	8.93	7.19	6.25	5.66	5.24	4.93	4.69	4.50	4.35	4.11	3.86	3.60	3.46	3.32	3.18	3.02	2.86	2.69
29	13.39	8.85	7.12	6.19	5.59	5.18	4.87	4.64	4.45	4.29	4.05	3.80	3.54	3.41	3.27	3.12	2.97	2.81	2.64
30	13.29	8.77	7.05	6.12	5.53	5.12	4.82	4.58	4.39	4.24	4.00	3.75	3.49	3.36	3.22	3.07	2.92	2.76	2.59
40	12.61	8.25	6.60	5.70	5.13	4.73	4.44	4.21	4.02	3.87	3.64	3.40	3.15	3.01	2.87	2.73	2.57	2.41	2.23
60	11.97	7.76	6.17	5.31	4.76	4.37	4.09	3.87	3.69	3.54	3.31	3.08	2.83	2.69	2.55	2.41	2.25	2.05	1.89
120	11.38	7.32	5.79	4.95	4.42	4.04	3.77	3.55	3.38	3.24	3.02	2.78	2.53	2.40	2.26	2.11	1.95	1.76	1.54
∞	10.83	6.91	5.42	4.62	4.10	3.74	3.47	3.27	3.10	2.96	2.74	2.51	2.27	2.13	1.99	1.84	1.66	1.45	1.00

v_1 and v_2 are the number of degrees of freedom in the numerator and denominator respectively.

The probability of F exceeding the entry value is in all cases 0.1%.

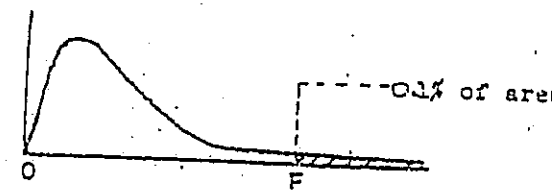


TABLE 08.4(B) : PERCENTAGE POINTS OF THE F DISTRIBUTION (UPPER .1% TAIL)